BoneSync™ Cement: A Biomechanical Analysis of Rotator Cuff Repair Augmentation in Open-Cell Foam Block

Arthrex Orthopedic Research

Background

Poor bone quality induces several challenges for arthroscopic rotator cuff repairs. Poor-quality bone of the proximal humerus can increase the chances of anchor pullout and require revisional surgery.¹ Calcium phosphate bone cement, such as BoneSync cement, can be useful for augmenting poor-quality bone.²

Materials and Methods

BoneSync cement has a set time of 6-10 minutes, and hardening occurs 24 hours postimplantation.² Several timepoints (0 minutes, 5 minutes, 10 minutes, and 24 hours) were selected to evaluate the fixation strength of Biocomposite 4.75 mm SwiveLock® anchors augmented with BoneSync cement throughout the hardening process. Timepoints were defined as the amount of time from the start of mixing until tensile testing was conducted.

Sample Preparations

Open-cell foam block was selected to mimic poor bone quality. A hole was punched into the 7.5 pcf open-cell foam block using a SwiveLock punch.

FiberTape® suture was threaded through the eyelet of a SwiveLock anchor to form a loop. For control group samples (no BoneSync cement), SwiveLock anchors were immediately inserted into the punched hole with the loop held around a 0.5-inch dowel rod.

For all other samples, BoneSync cement was mixed with 0.8 cc phosphate-buffered saline (PBS) according to the packaging instructions. The mixture was injected into the punched hole using a delivery cannula, and then the SwiveLock anchor was inserted directly following injection (Figure 1).

Each sample was closed in a jar of PBS and placed in a 37 °C (body temperature) environmental chamber for a set amount of time (5 minutes, 10 minutes, or 24 hours). Zero-minute timepoint samples were not immersed in PBS.

Figure 1. Prepared BoneSync cement sample

Tensile Testing Method

Once removed from the PBS, the suture loop was attached to a hook and the foam block was secured under a box fixture. A preload of ~0.1 N was applied. Following the preload, tensile testing was performed at a rate of 5 mm/s until failure. The maximum load (up to 3 mm of displacement), displacement at maximum load, and failure mode were recorded.

Results

The maximum load was defined as the maximum load achieved at or before 3 mm displacement. Displacement at 3 mm was used to represent clinical failure for this application.

Figure 2 shows the mean maximum load at each time point. Significant differences were found between the control group and 10-minute ($P = .009$) and 24-hour (P < .001) timepoints. The failure mode for all samples was anchor pullout (Figure 3).

Figure 2. Maximum load at or before 3 mm of displacement for each timepoint³

Table 1. Maximum Load Data (Mean ± SD)³

Figure 3. Failure mode for all samples was anchor pullout

Conclusions

The presented porous sawbones model with BoneSync™ augmentation demonstrates significantly higher ultimate loads at the 10-minute and 24-hour timepoints compared to the models without BoneSync augmentation. The time-zero analysis provides evidence that BoneSync augmentation in poor-quality bone may be more resistant to pullout forces after the specified setting time.

References

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